

## WELCOME

21-JUNE -2023

**Tech TANGENT Solutions Pvt. Ltd.** 

An Engineer is a person who applies the basic knowledge of science for the good of society.

## **Session 9**

## Wind Engineering Studies for Long-Span Bridges

# By Dr. SURESH KUMAR Vice President Global Consulting



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### Dr. SURESH KUMAR - Vice President Global Consulting



- ✤ Education
- Postdoctoral studies, Eindhoven University of Technology, Eindhoven, The Netherlands.
- Doctor of Philosophy, Concordia University, Montreal, Canada
- Master of Science (Engineering), Indian Institute of Science, Bangalore, India
- Dr. Suresh Kumar based in London, UK, is well recognized leader in the field of wind engineering.
- He has over 32 years of experience as a wind engineering researcher and consultant internationally.
- ✤ He has been with RWDI for the past 21 years.
- He has directed the establishment of RWDI's 5th wind tunnel in Trivandrum, India.
- He has worked as a wind consultant on many iconic structures worldwide, including the world's tallest tower, the Burj Khalifa in Dubai.
- He has published or presented numerous papers in international journals and conferences.
- He is also very active in professional organizations around the world.

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# RWDI's Key Experiences

BRIDGE NAME	SPAN (m)	LOCATION
Messina Strait (Suspension)	3300	Sicily to Calabria, Ita y
Golden Gate Bridge (Suspension)	1280	San Franciscu, CA, USA
Stonecutters Bridge (Cable- Stayed)	020	Pong Kong, China
Tacoma Narrows (Susrension)	853	Tacoma, USA
Millau Viaduct (Cable Stavua)	342	Millau, France
	HEIGHT (m)	LOCATION
Kingdom Tower	1000	Jeddah, Saudi Arabia
Burj Khalifa	828	Dubai, UAE
Shanghai Tower	632	Shanghai, China





## Outline

- Introduction
- Wind Climate Analysis (for deck, pylons, cables)
- Desktop Stability Assessment (for deck, pylons)
- Sectional Wodel Test (for deck)
- **Construction of the second se**
- Concluding Remarks

**Future Webinar:** 

Aeroelastic wind tunnel study, Vehicle-induced vibrations, Pedestrian-induced vibrations, Supplementary damping considerations, Cable stability analysis, Full-scale measurements, Health monitoring and retrofitting.



#### Introduction

Tacoma Narrows: Span/Width – 1:72 Span/Depth - 1:35 Weight 4.25 thin CN ( Tacoma Narrows, Washington, USA **Golden Gate:** Span/Width - 1:16 Span Deptl Weight -



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#### Introduction

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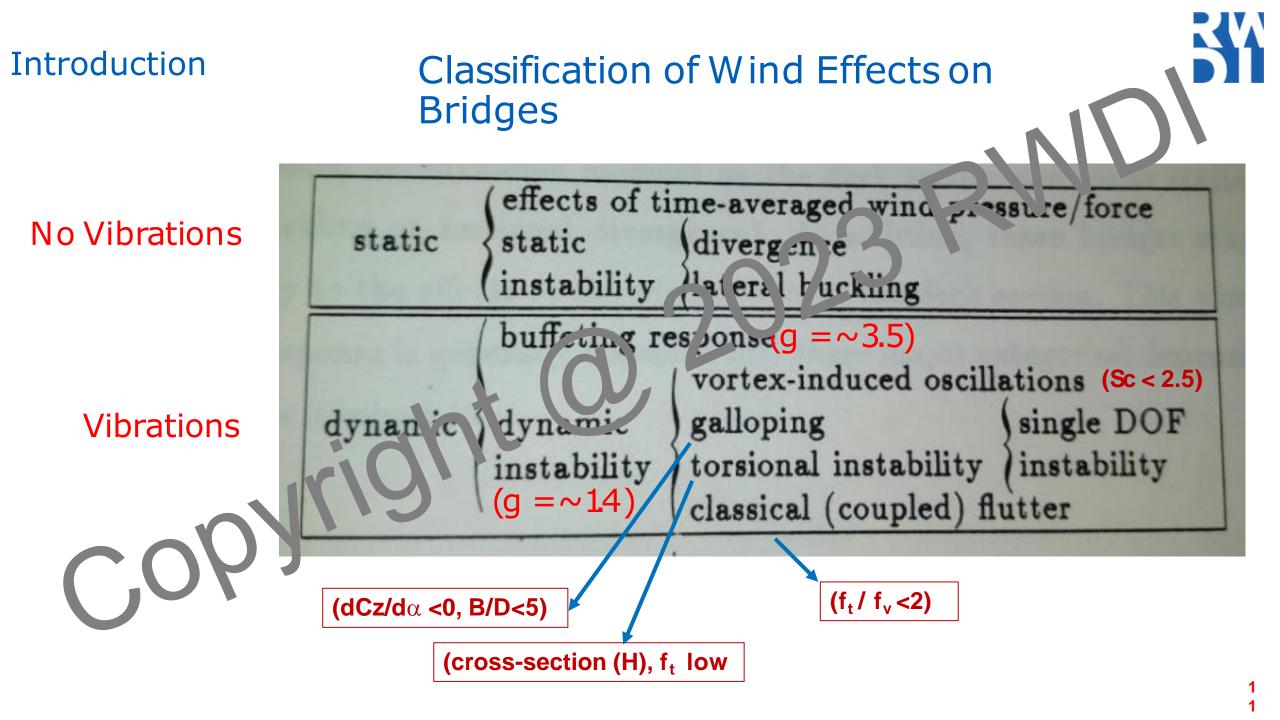
- Light Weight (10 50 ton/m) ; Pedestrian (<5 ton/m)
- Supports only at ends (Contrary to tall buildings where having dv intage)

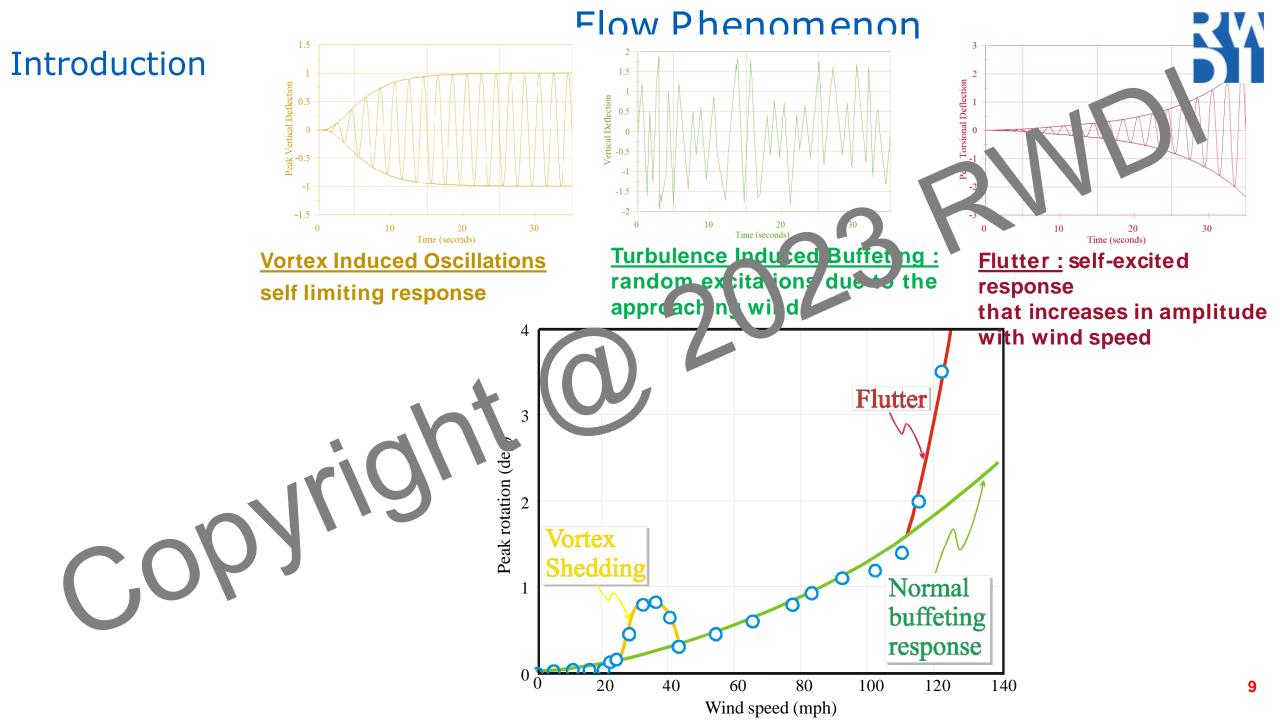
550 ton

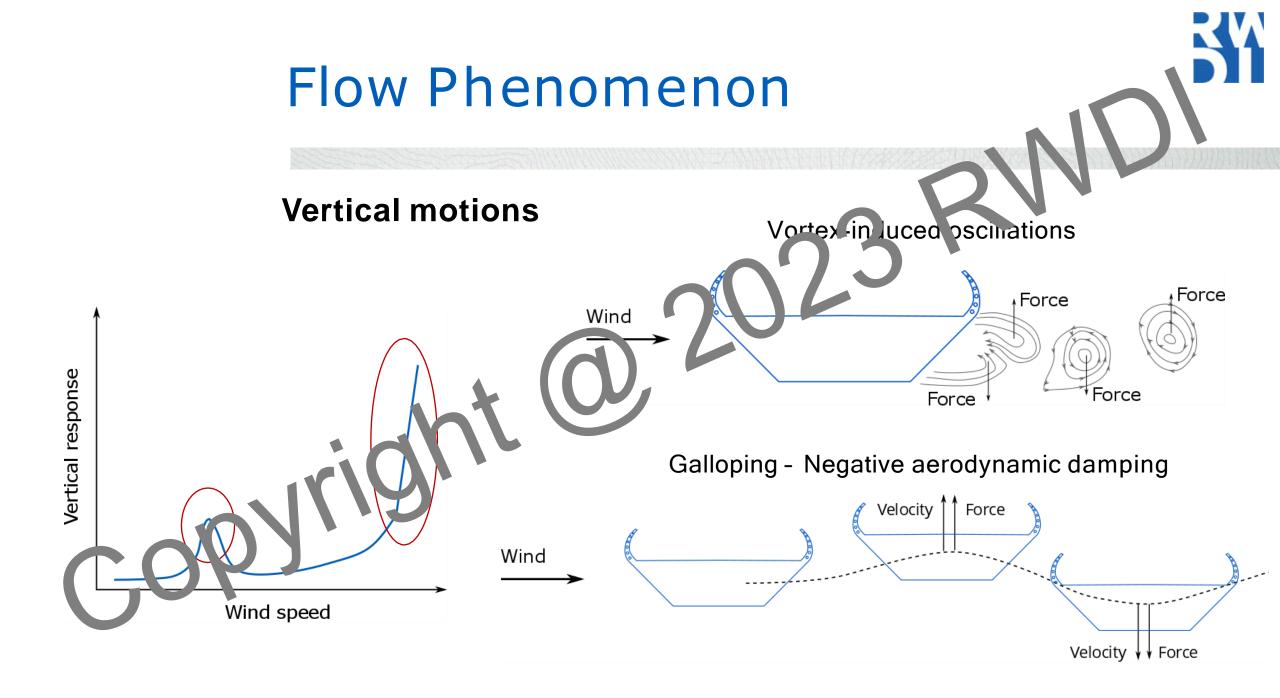


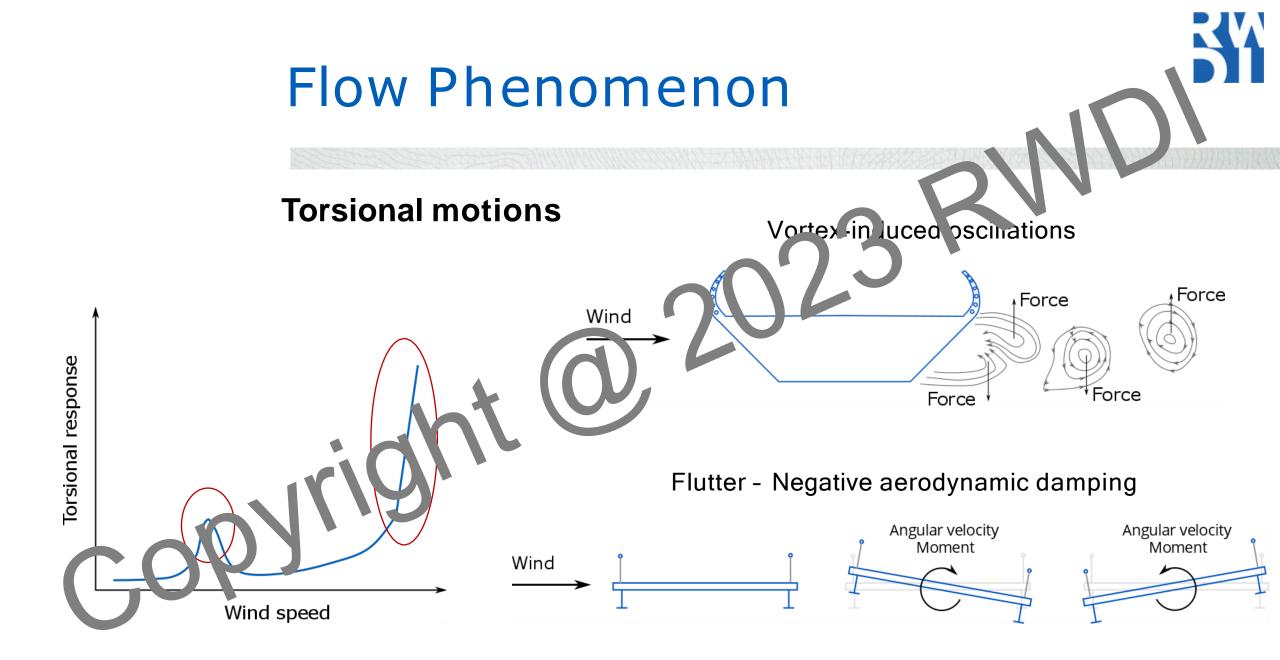
Weight - 100,000 ton

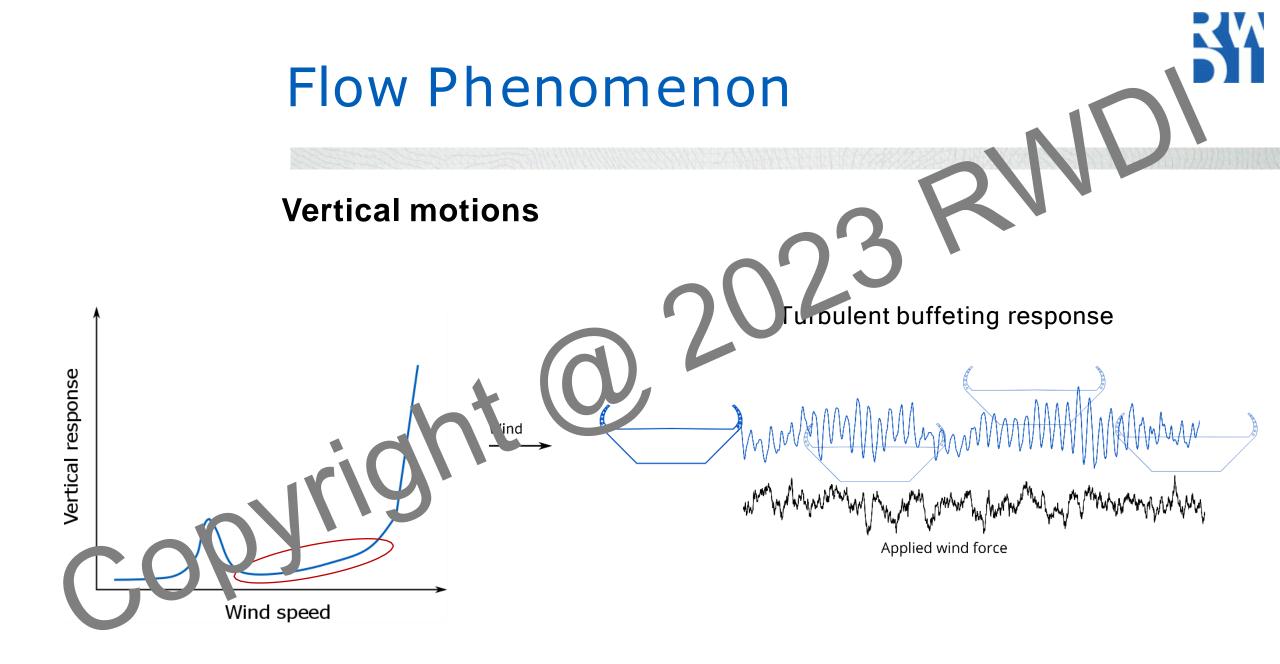
Weight  $\sim$  1500 ton/floor (500 ton/m)



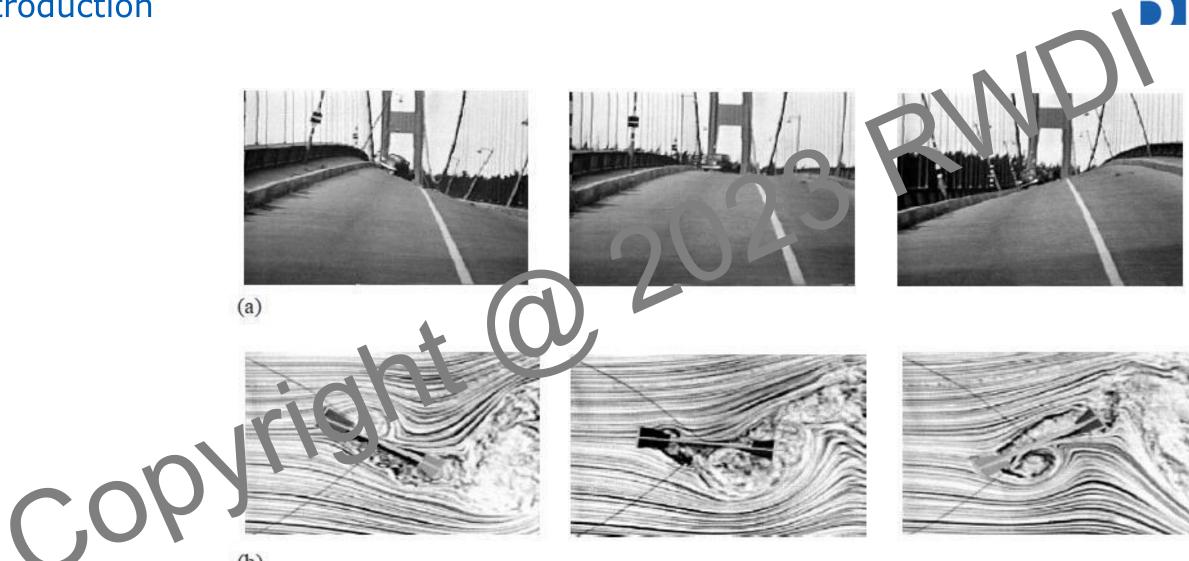






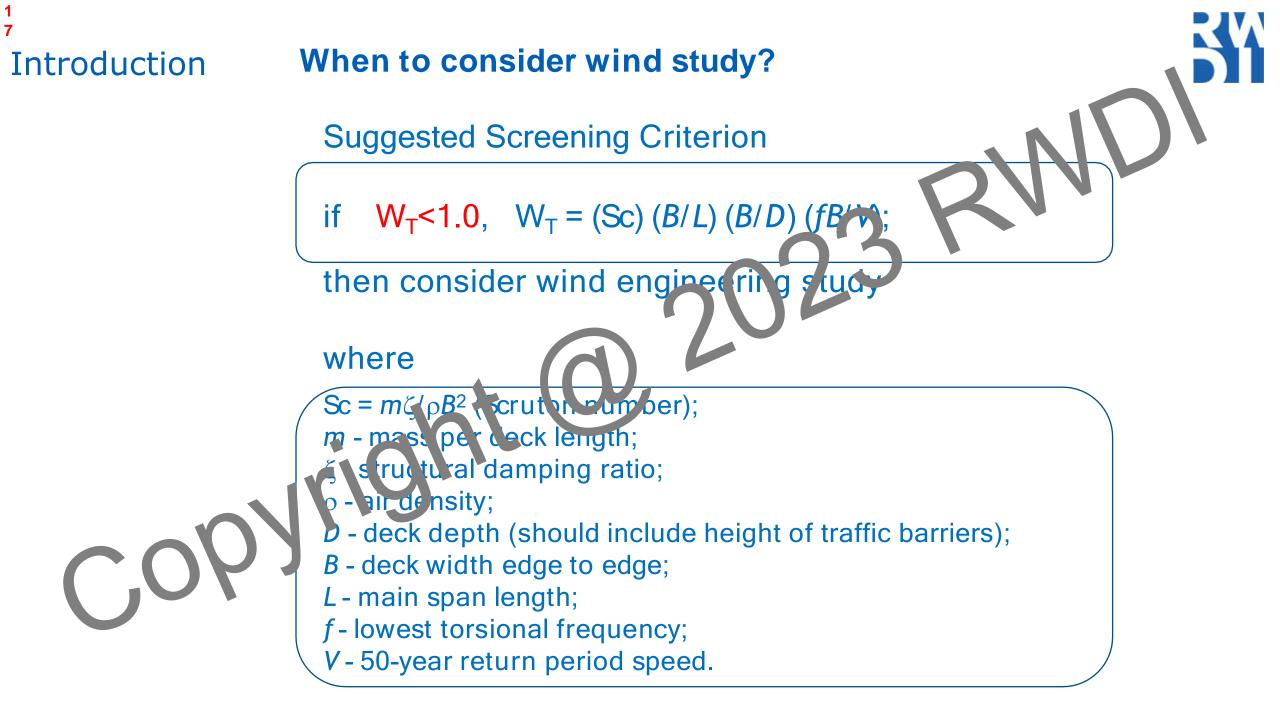


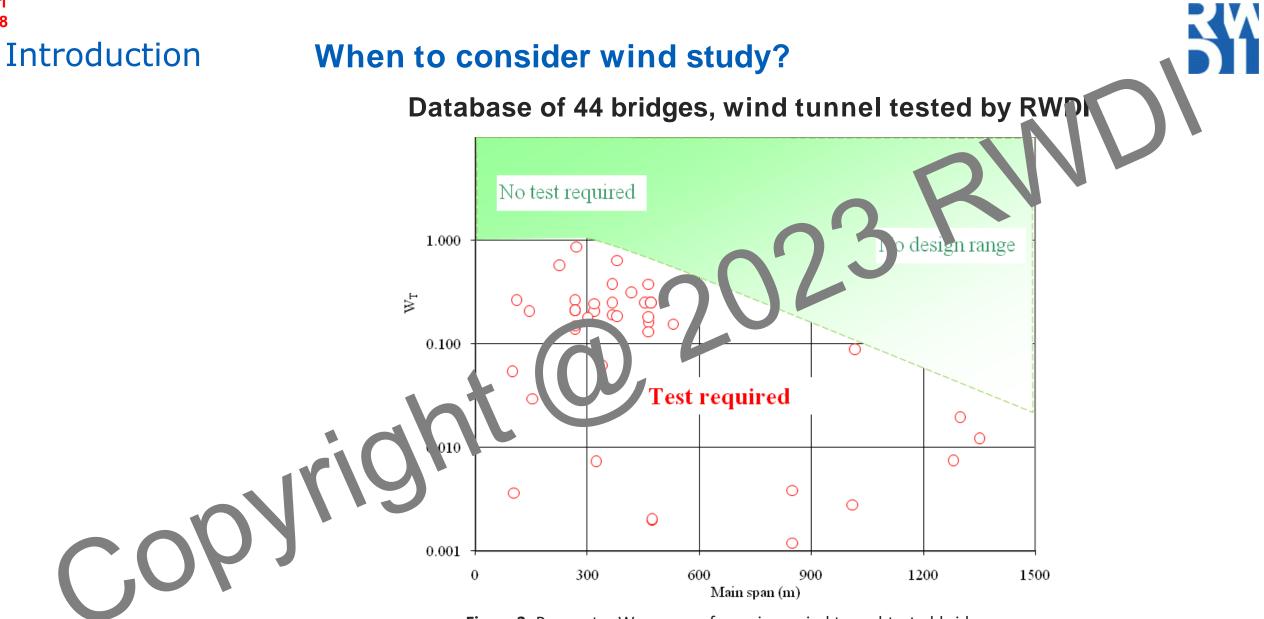
# Introduction



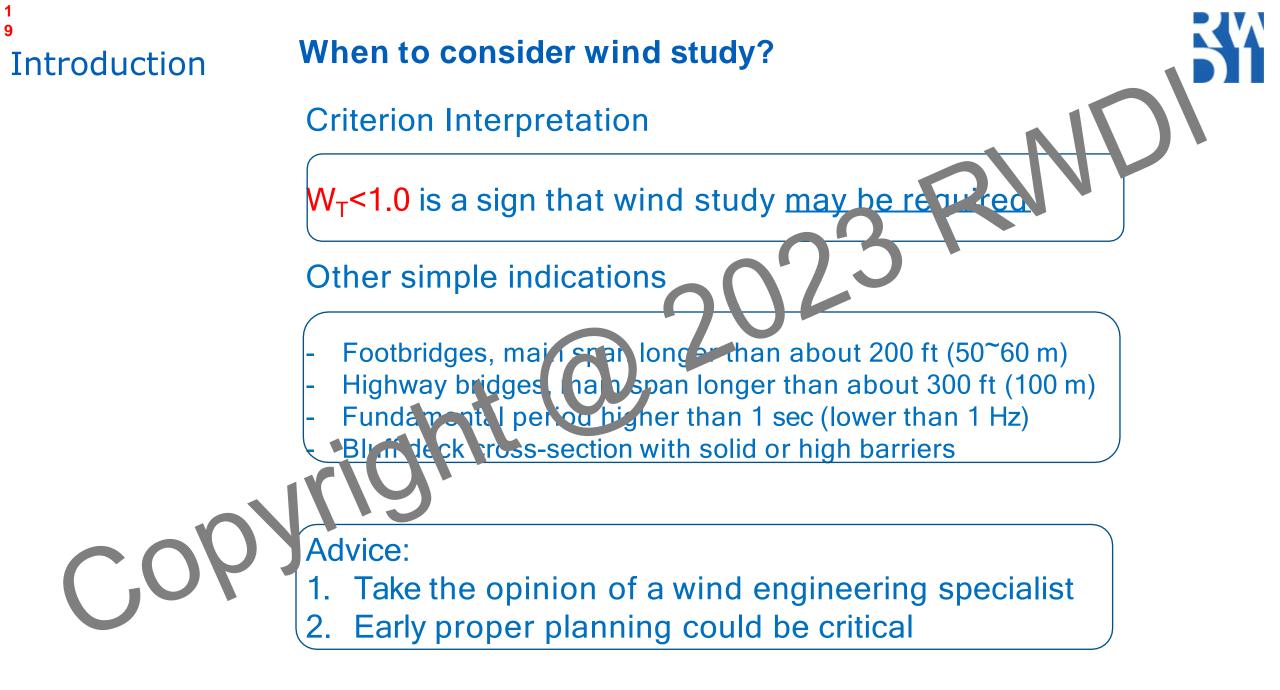
**Flow Phenomenon** 

(b)





**Figure 3:** Parameter W<sub>T</sub> vs. span for various wind tunnel tested bridges



#### Essential wind engineering studies required are

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Introduction

Wind climate analysis - wind characteristics required for ther fication of aerodynamic stability and derivation of design loads

Desktop stability assessment - performed to verify stability of bridge at early stages of planning

Sectional model test - performed to verify the stability of the bridge, unacceptable motions, mitigation measures, force coefficients

Buffeting analysis - analytical simulations to determine structural responses & load distributions



#### Wind speed vs return period

 Meteorological data from airports, werther stations, masts, balloon data etc.

Influence

of Terrain

THE ALAN G. DAVENPORT WIND LOADING CHAIN

Aerodynamic

Effects

Dynamic

Effects

Criteria

Reliability of existing date??

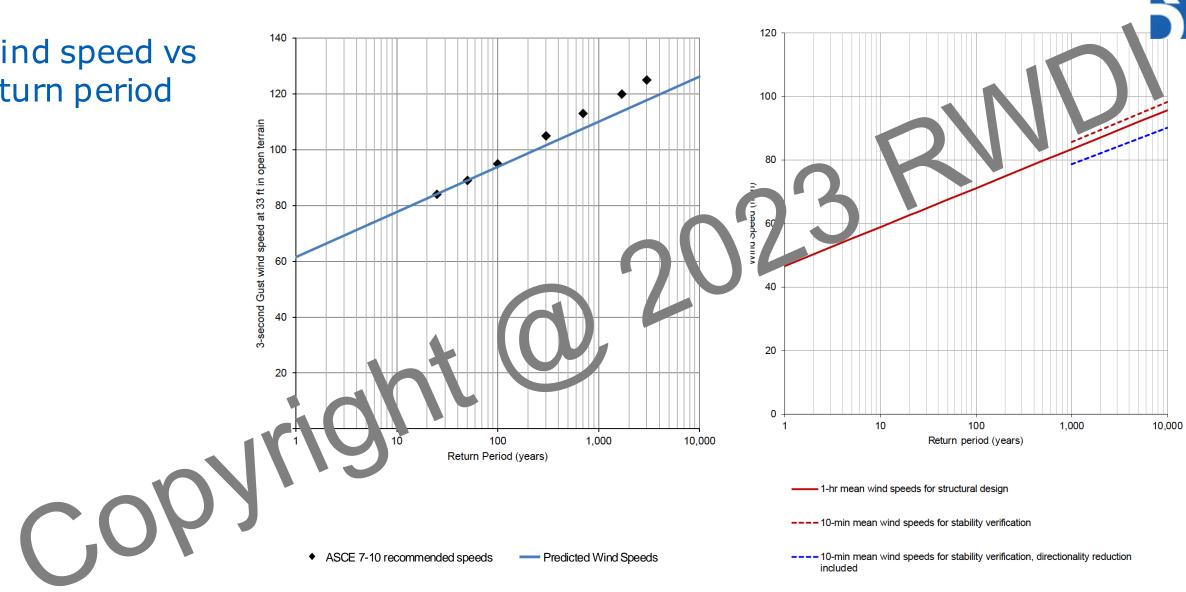
WIND LOAD

Wind

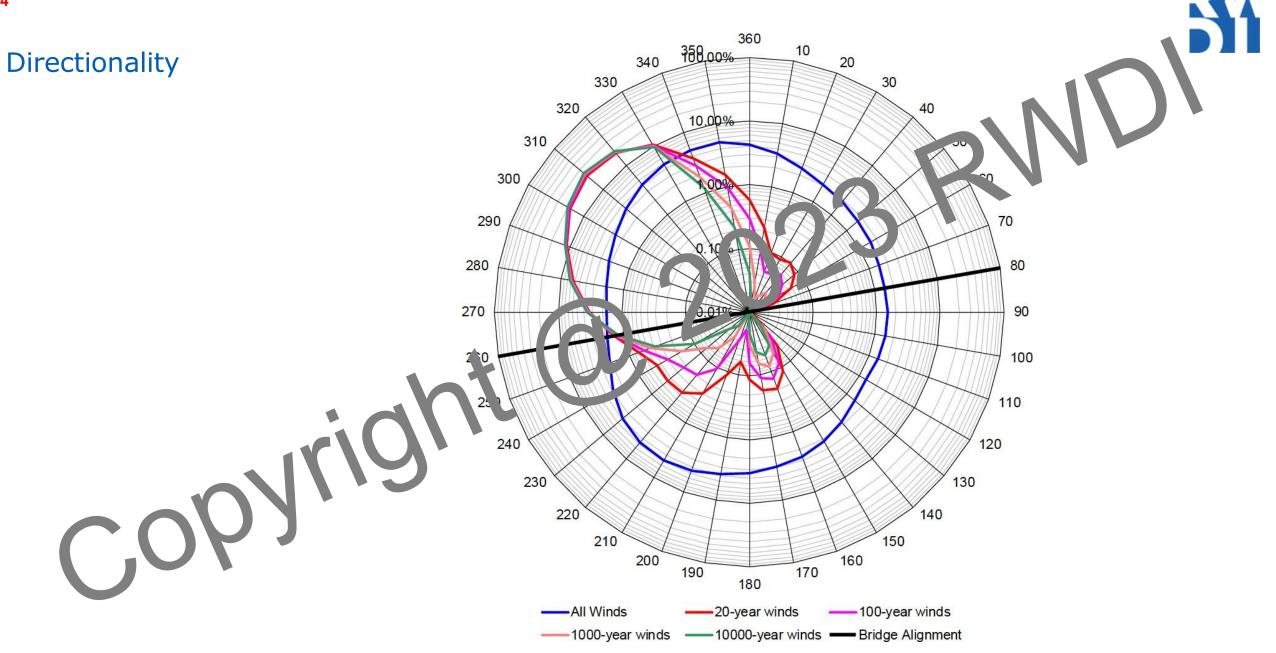
Climate

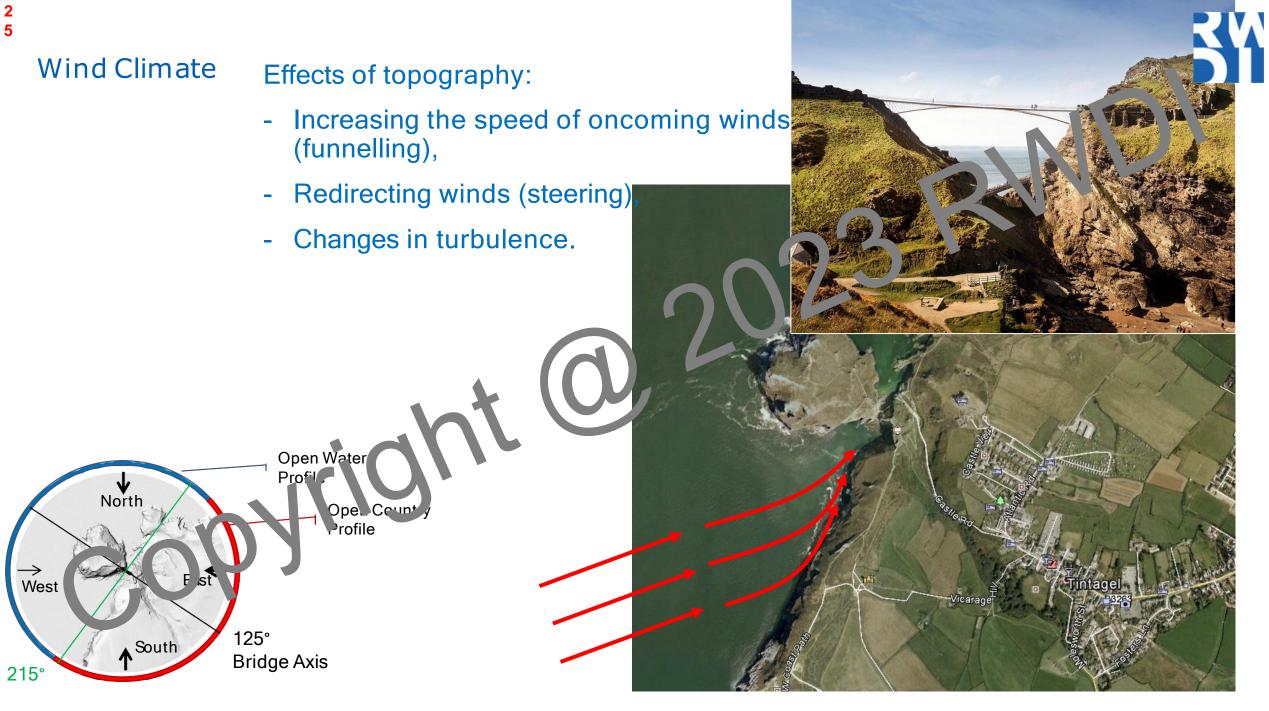
- Monte-Carlo basec c/clon c simulations are essential for the coastal regions in trop cal clinates in the absence of real measurements
- WRF numerical modeling could be adopted to simulate a large set of nata for the interior regions of India (absence of data & topographical effects)
- Return Periods 20, 100, 1000, 10000
- Uncertainty in speeds leads to conservative assumptions elevate design demands, uneconomical structures

#### Wind speed vs return period



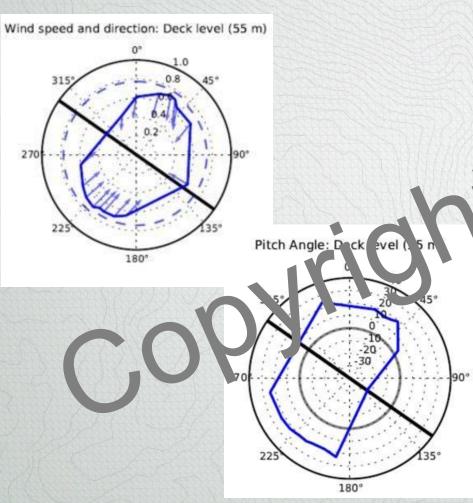


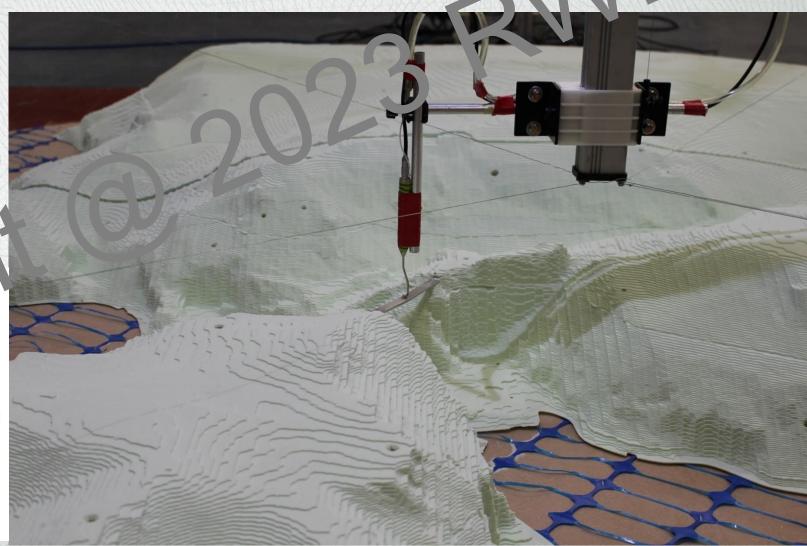




## Wind Climate

#### **Detailed topography tests:**

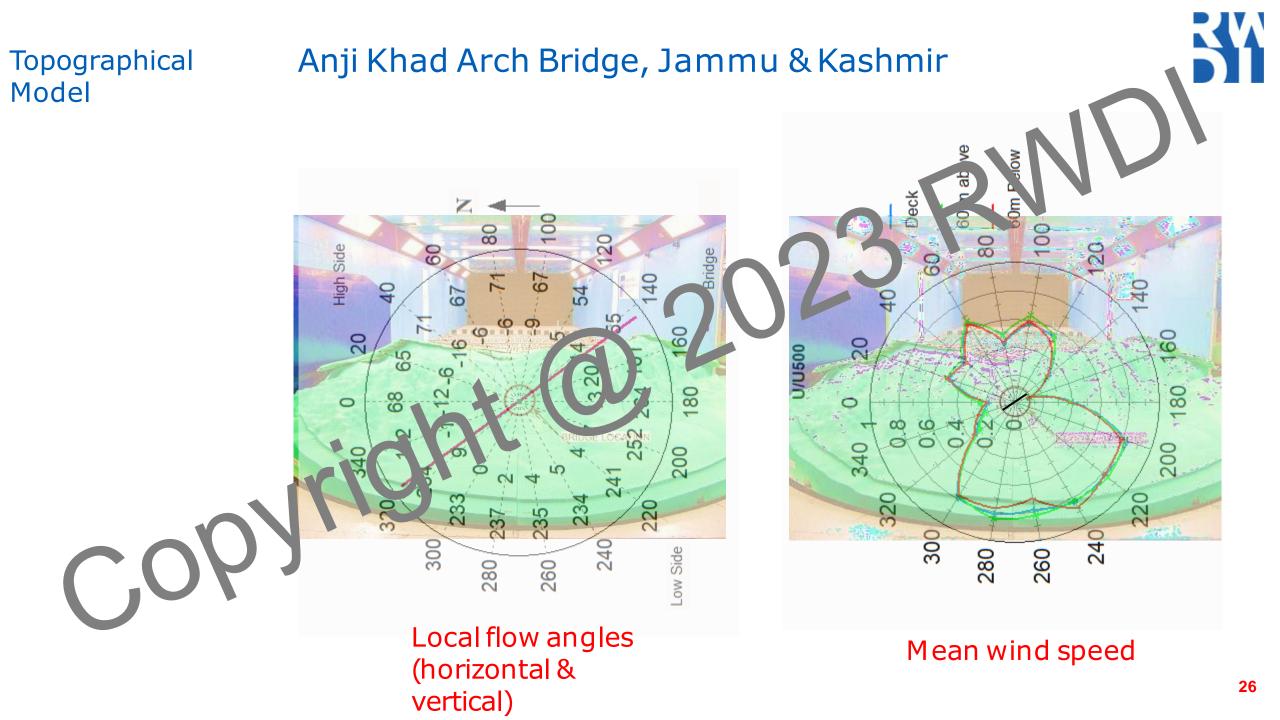




## Complex surroundings



## Anji Khad Arch Bridge, Jammu & Kashmir Topographical Model BRIDGE LOCATION C0/ 240 270 --1



#### <sup>3</sup> Topographical Model

#### Anji Khad Arch Bridge, Jammu & Kashmir

 Table 1: Design Wind Speeds for the Anji Khad Arch Bridge

	Return Period	Application	A	Col resp. nding Wind Speed at Deck Height (m/s)			
	(years)		Sec nd Gi et	Mean Hourly	10-Minute Mean	3-Second Gust	
	10	Construction Stope Loading	32.4	28.3	30.0	41.1	
	50	Basic De ig n Win I Speed – IS 9/5	39.0	34.0	36.1	49.5	
	100	tructural Design of Completed Bridge	41.4	36.1	38.3	52.5	
	0.0	Stability - Construction Stage	50.4	43.9	46.6	63.9	
$\cdot 0$	10000	Stability - Completed Bridge	59.3	51.8	54.9	75.3	
Note: $A = Wind speed at 10 m in Category 2 terrain (m/s)$							

NDI

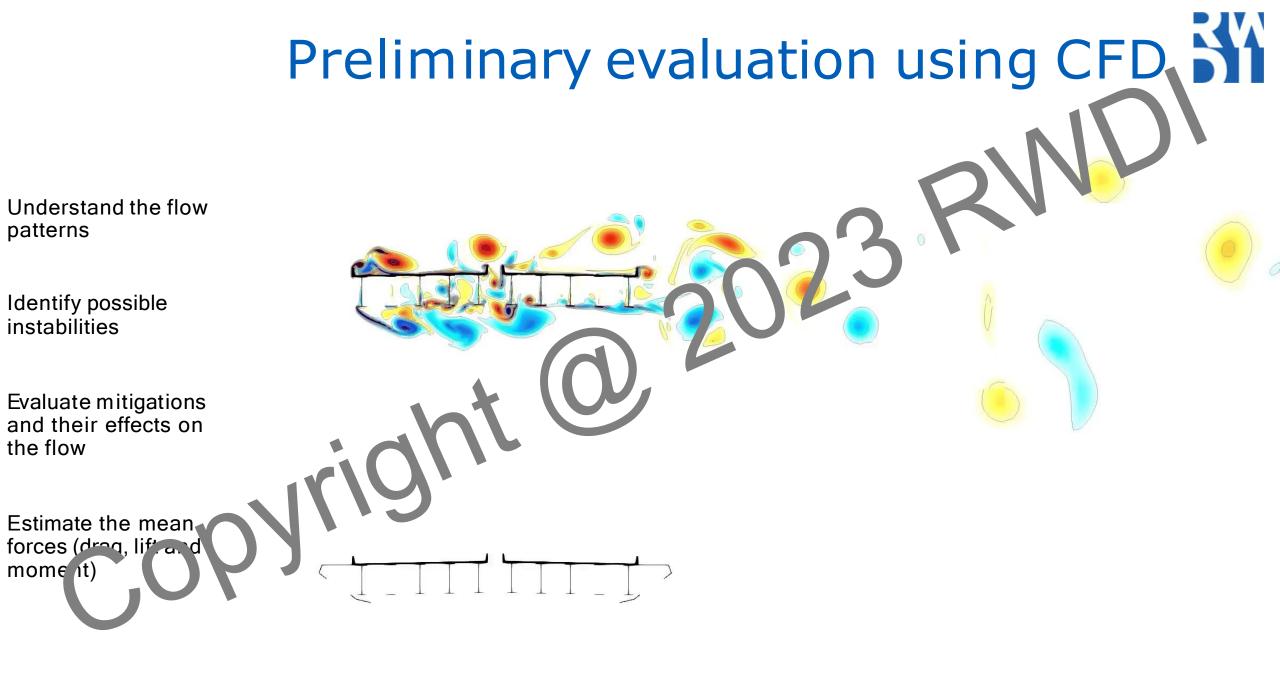


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Desktop Stability Assessment

CODIL

- Analytical calculations based on past experience and RWD
   database of past wind tunnel tests
- Early notification of potential problems, and identity way forward
- May require simple 2D CFL studies if deck geometry is unusual



#### Recent study – using CFD and sectional model tests

C<sub>d</sub>: +7% *versus* baseline configuration

2.5-r. i eight nvelope

Concounding to 66% of the free stream velocity

(FD con jive early indications and reduce the number of wind tunnel

tesis

0.50 0.00 0.50 1.00 1.50

 $U/U_{ref}$ 



#### **Stability Design Criteria** Sectional Model Test 1,000-year return period, zero agle a wind incidence **Flutter Construction:** Onset speed > 1000-y-ar return period speed at bridge deck **Completed:** rear return period, zero angle of wind incidence 10,0,0 Onset speed > 10000-year return period speed at bridge deck For highe s of attack, one can reduce wind speed criteria ( $\sim$ 20%) ngl of flucter if the torsional amplitude exceeds 1.5 degrees Vortex 5% of gravity up to 30 mph (13 m/s) (1.8% g for tall buildings) Shedding 10% of gravity from 30 to 50 mph (22 m/s). Induced If above 50 mph - become a strength or fatigue issue, not comfort 33 Oscillations

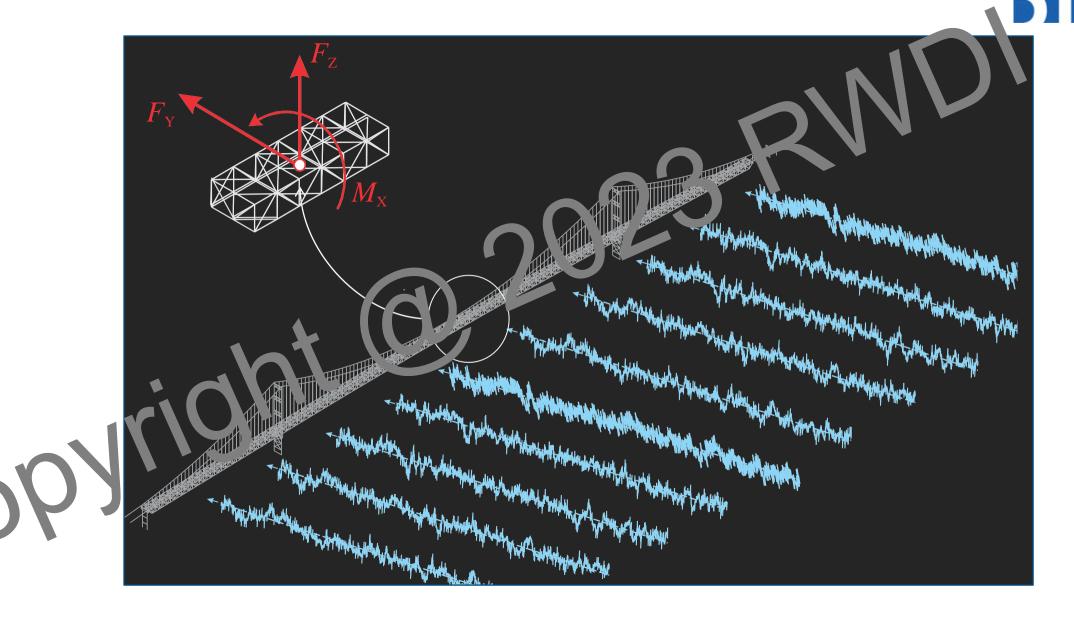
, Sectional Model Test

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- Pass or Fail Test
- Carried out at the preliminary design stage to assess the verodynamic stability of the deck section
- Aerodynamic Phenomenon: Firster, Voitex Snedding, Buffeting
- In case of instability remedia measures will be suggested and confirmed through wird tunnel tests. The wind tunnel becomes a design tool provided endence of the performance of a geometry and a mitigation solution

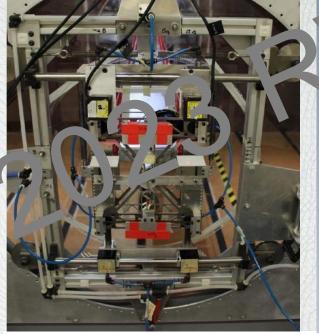
Other results once stability confirmed: Static coefficients, aerodynamic derivatives

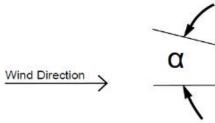
Sectional Model Test

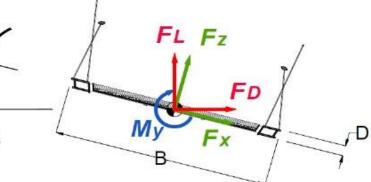


## Sectional Modal Test





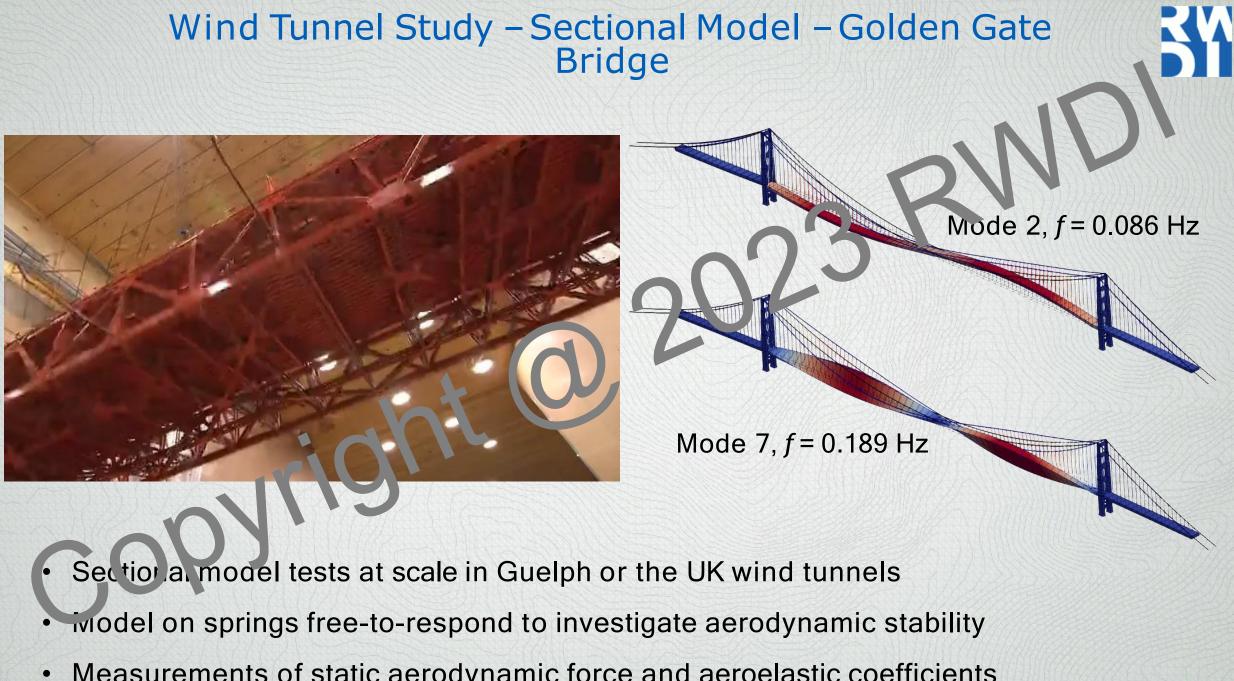






# Sectional model test

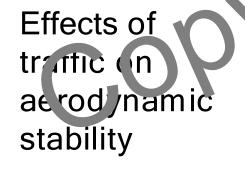


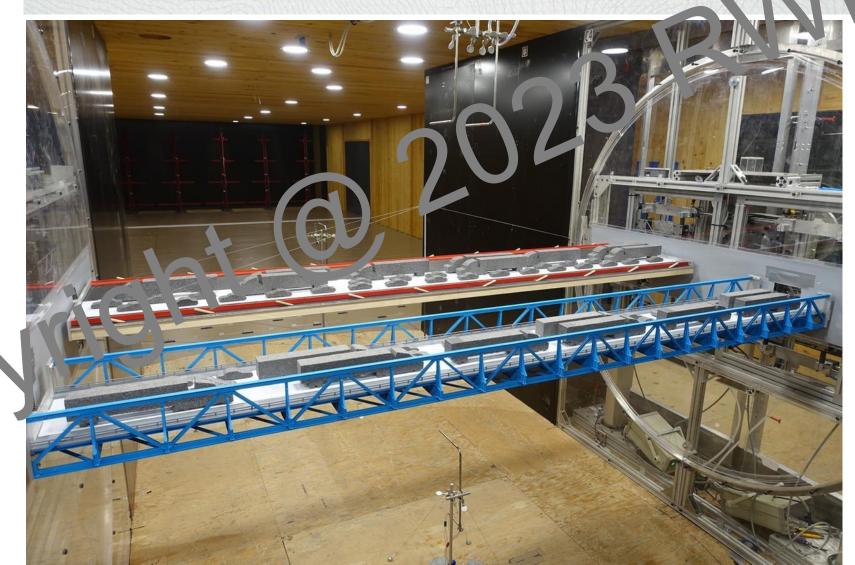


Measurements of static aerodynamic force and aeroelastic coefficients

# Sectional model test, twin bridges

Interference effects between bridges





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#### Twin deck sectional model tests

CO



₄ Sectional Model Test

- Sectional models rigid and geometrically represent a segment of the full-scale deck
- Typical geometrical scales are in the range of 1:30 ~ 1:80
- Materials used for construction: Brass, Aluminum, Wood, Plexiglass

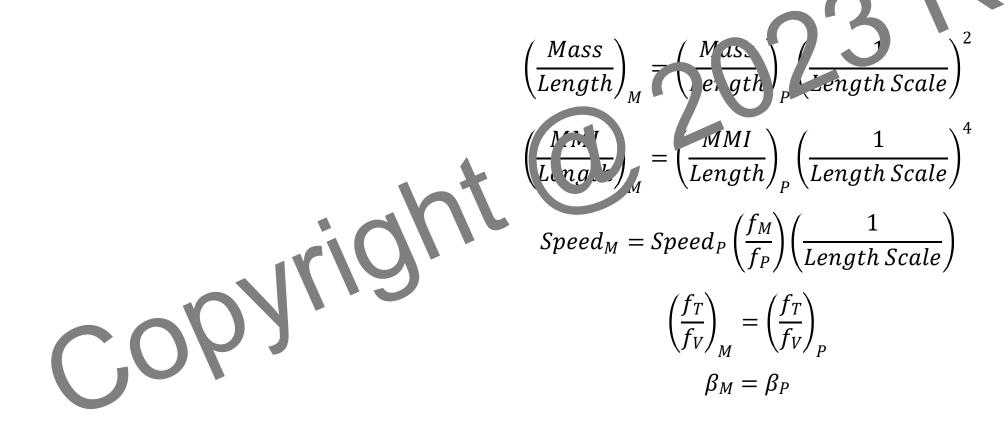
Non-dimensional parameters

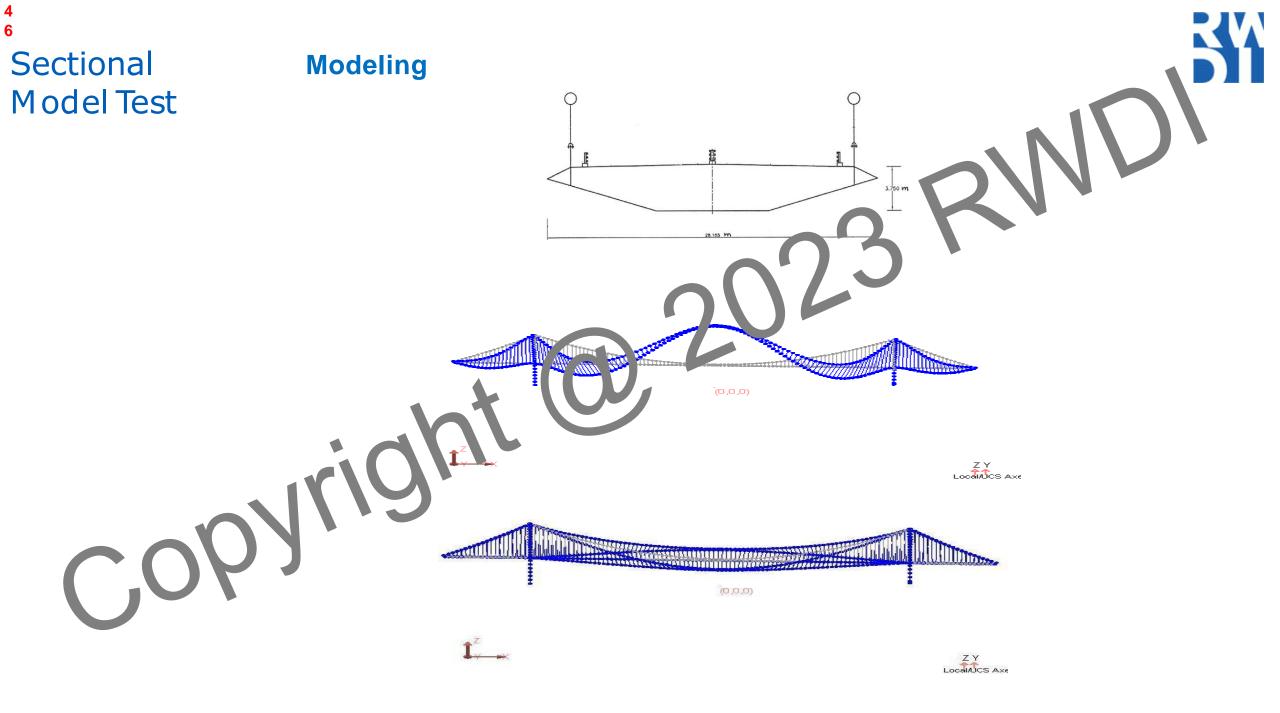






- Geometric Similarity
- Kinematic Similarity (Partial turbulence simulation)
- Dynamic Similarity

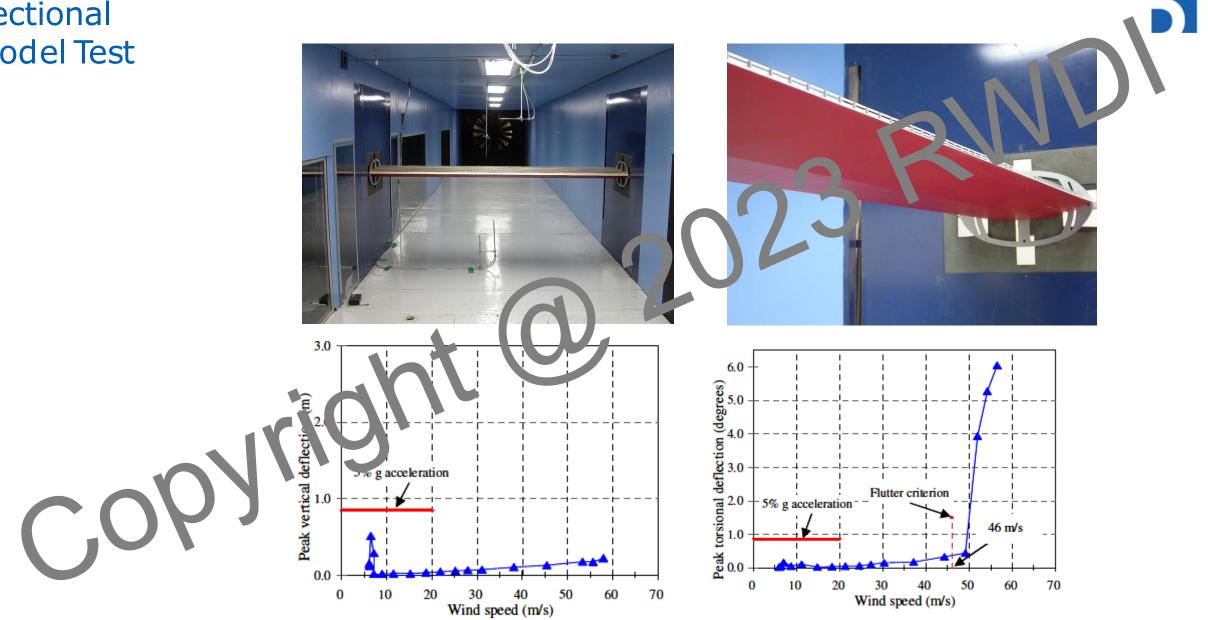


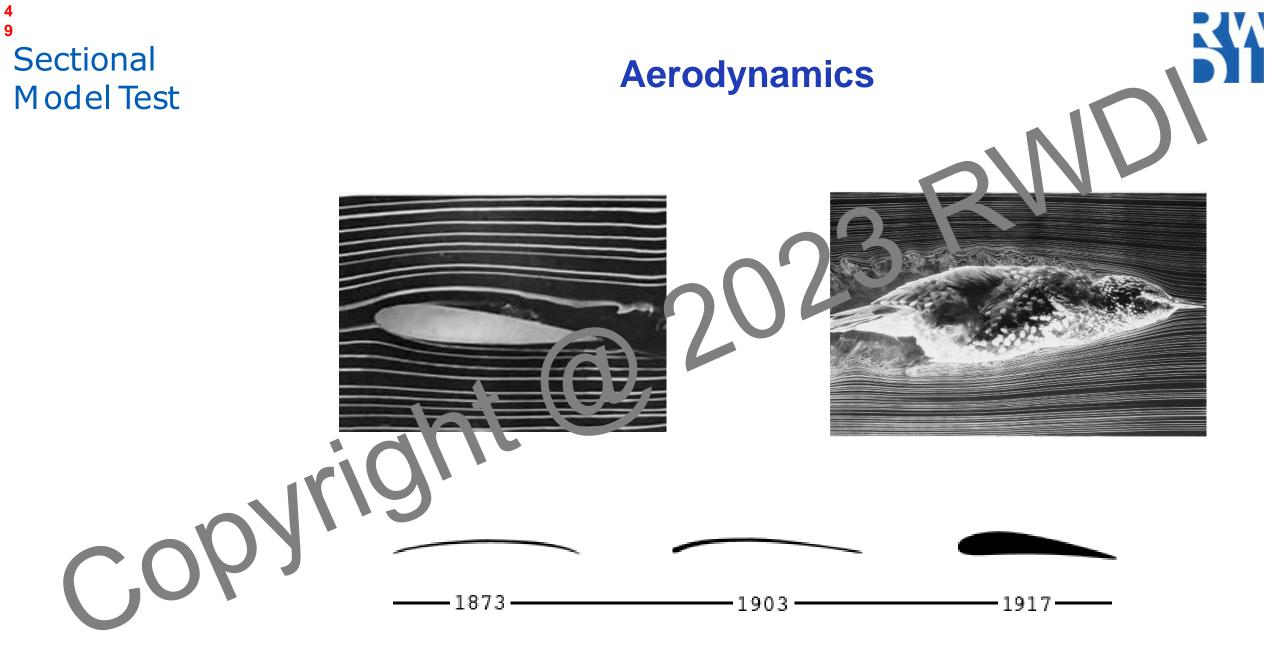


## Sectional Key parameters of the sectional model Model Test

	Key Parameter	Full Scale	▶ odel ∑ale 1:60	
		03	Target	Actual
	Vertical frequency	0121Hz		1.53
	Torsional frequency	047 Iz		4.5
	Frequency ratio	2.87	2.87	2.94
	Deck mass + 2x Cable	17,600+2x 2800 kg/m	15.47 kg	15.4 kg
	Deck mass moment of iner ca (mmi)	1,041,000 kg.m <sup>2</sup> /m	0.193 kg.m <sup>2</sup>	0.240 kg.m <sup>2</sup>
	Equivale t Lami, Mode 19	2,067,000 kg.m <sup>2</sup> /m	0.383 kg.m <sup>2</sup>	
	Vertical clamping	0.2 ~0.3 %	0.2~0.3 %	0.25 %
$\sim$	Torsional damping	0.2~0.3 %	0.2~0.3 %	0.30 %

Sectional Model Test

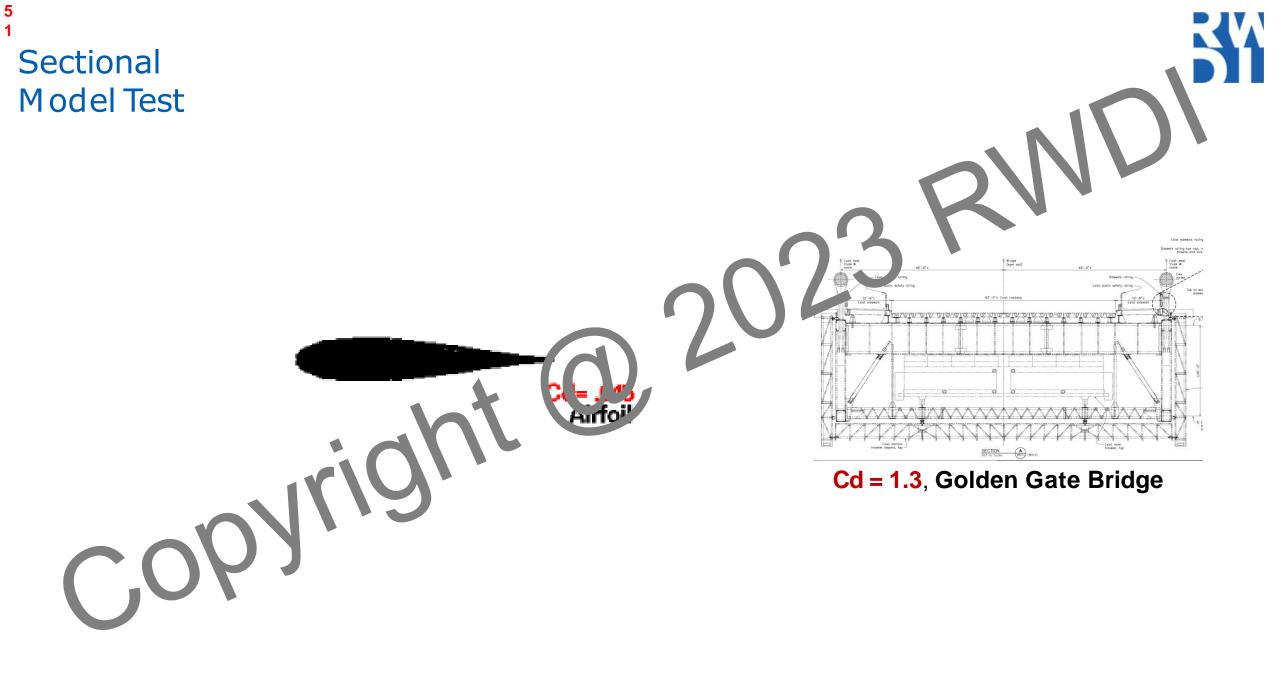




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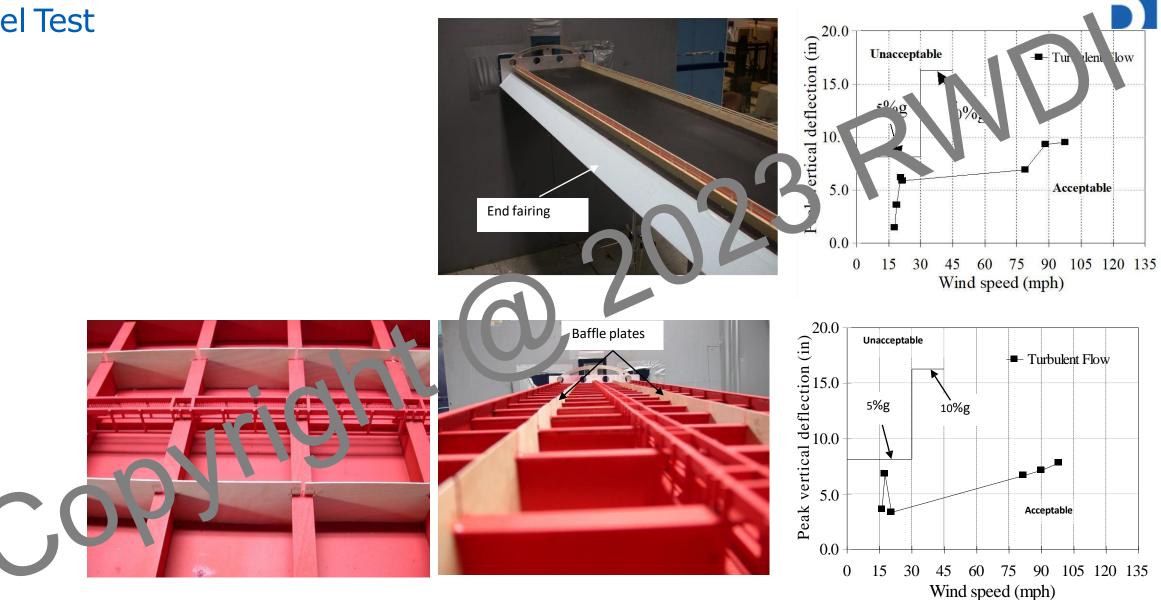
Model Test

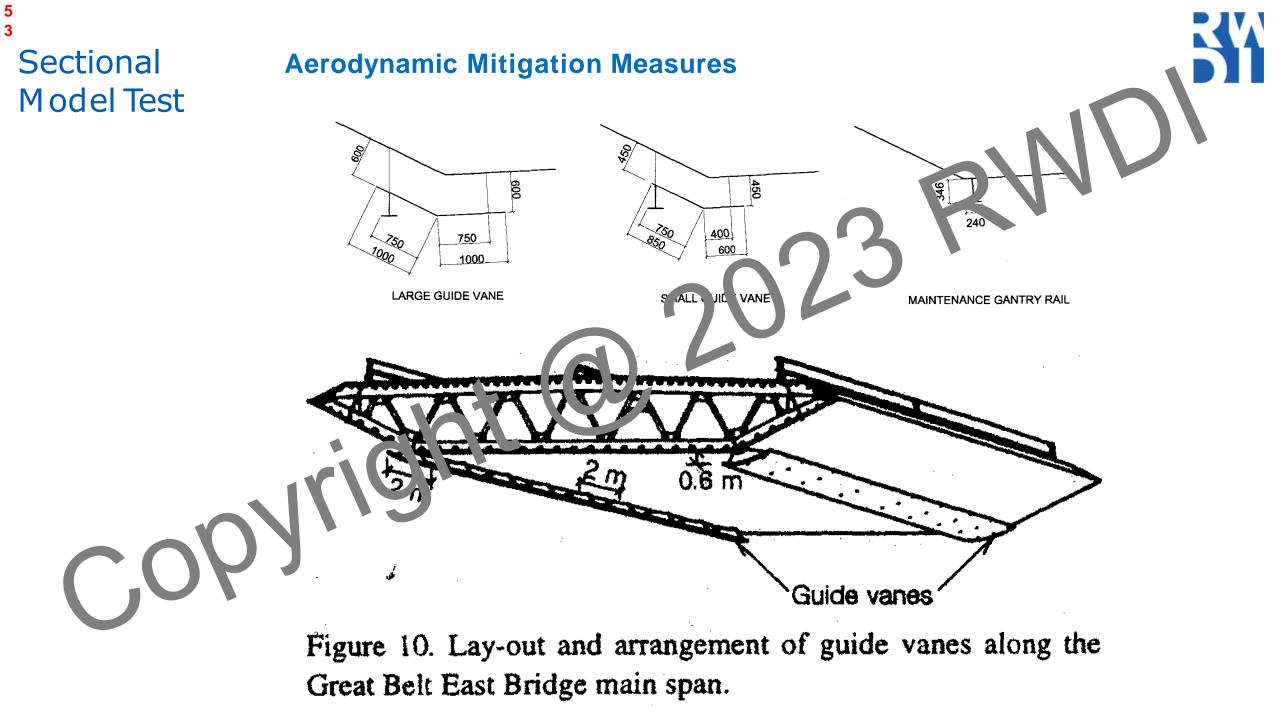




#### <sup>5</sup> <sup>2</sup>Sectional Model Test

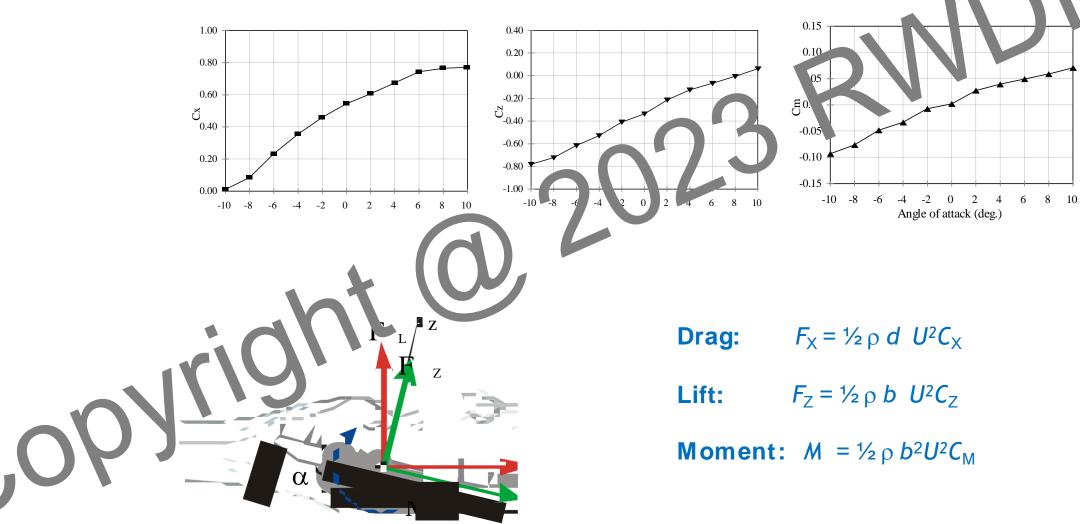
#### **Aerodynamic Mitigation Measures**





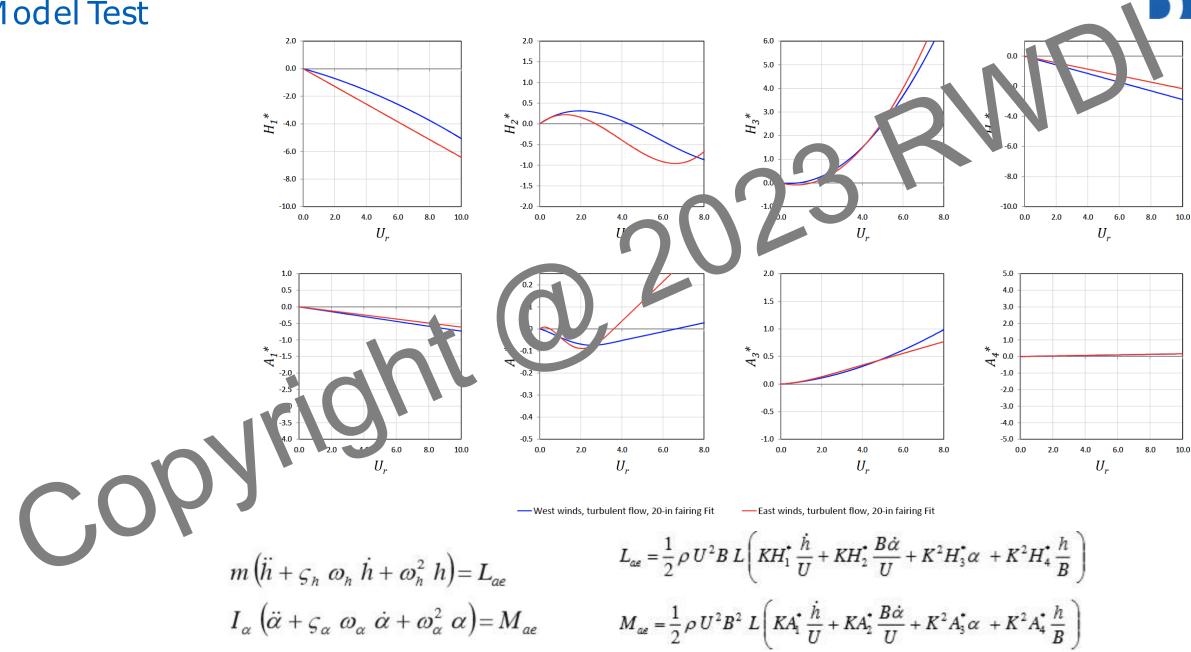
## Sectional Model Test

#### **Force and Moment Coefficients**





#### **Aerodynamic Derivatives**





# For the second secon

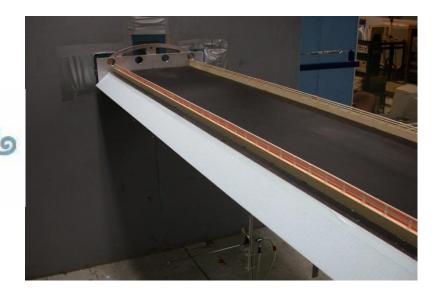
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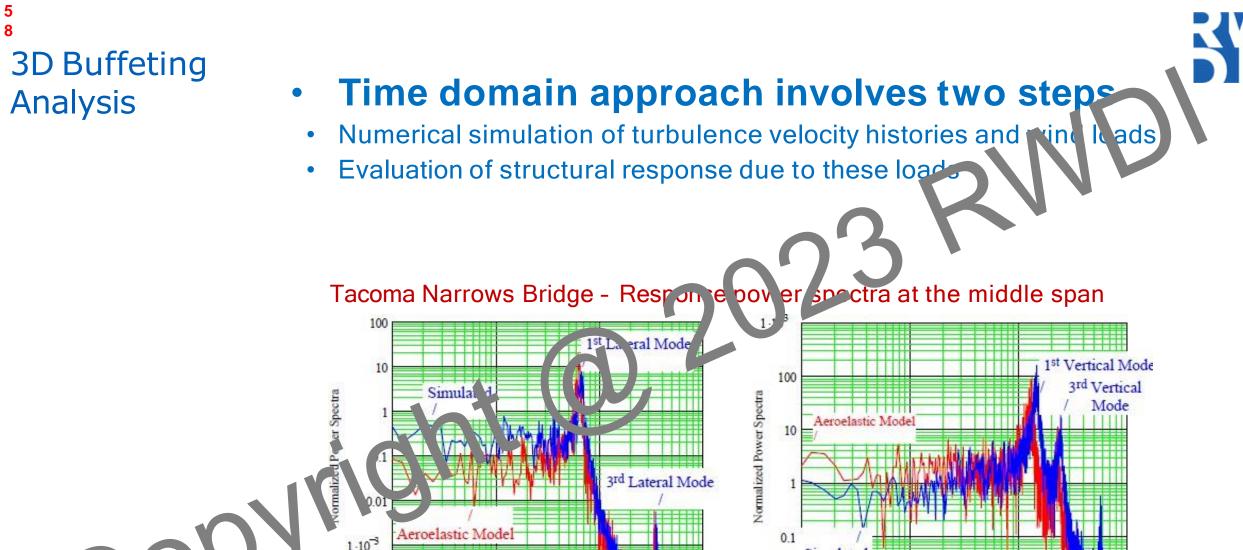
## Statistical predictions of peak responses

Direct integration of dynamic equations of motion in time counain

### • Inputs

- Static aerodynamic force & moment coefficients
- Mass and MMI
- Bridge dimensions
- Mode shape & irequancies
  - Structural camping
  - Vind turbulence properties
  - erod /namic derivatives





 $1.10^{-4}_{1.10}$ , 0.01, 0.1, 1Frequency (Hz) a) power spectra of lateral deflections

b) power spectra of vertical deflections

Frequency (Hz)

0.1

0.01

Simulated

0.01

## Evaluating the buffeting motion to derive wind loads

0.5

0.3

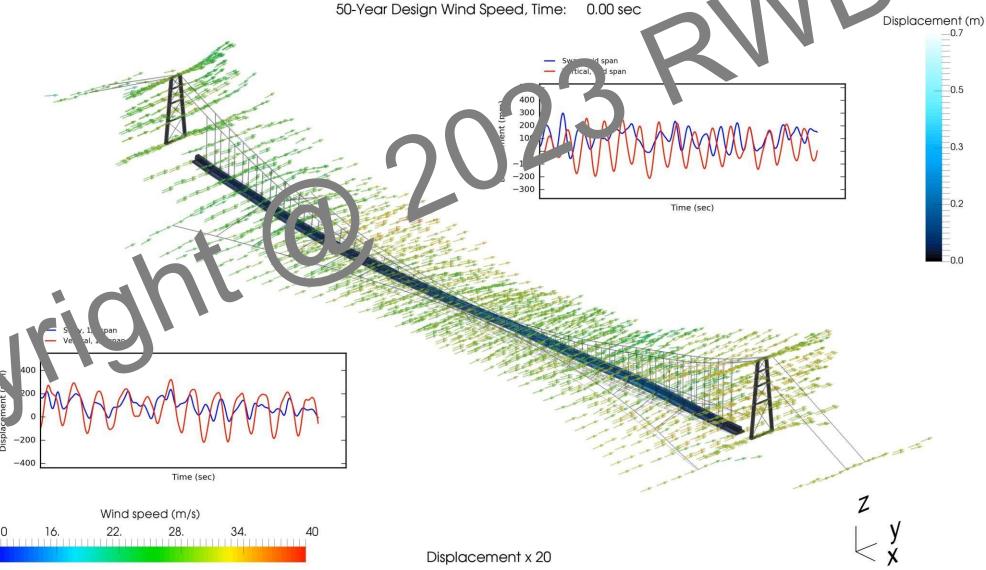
0.2

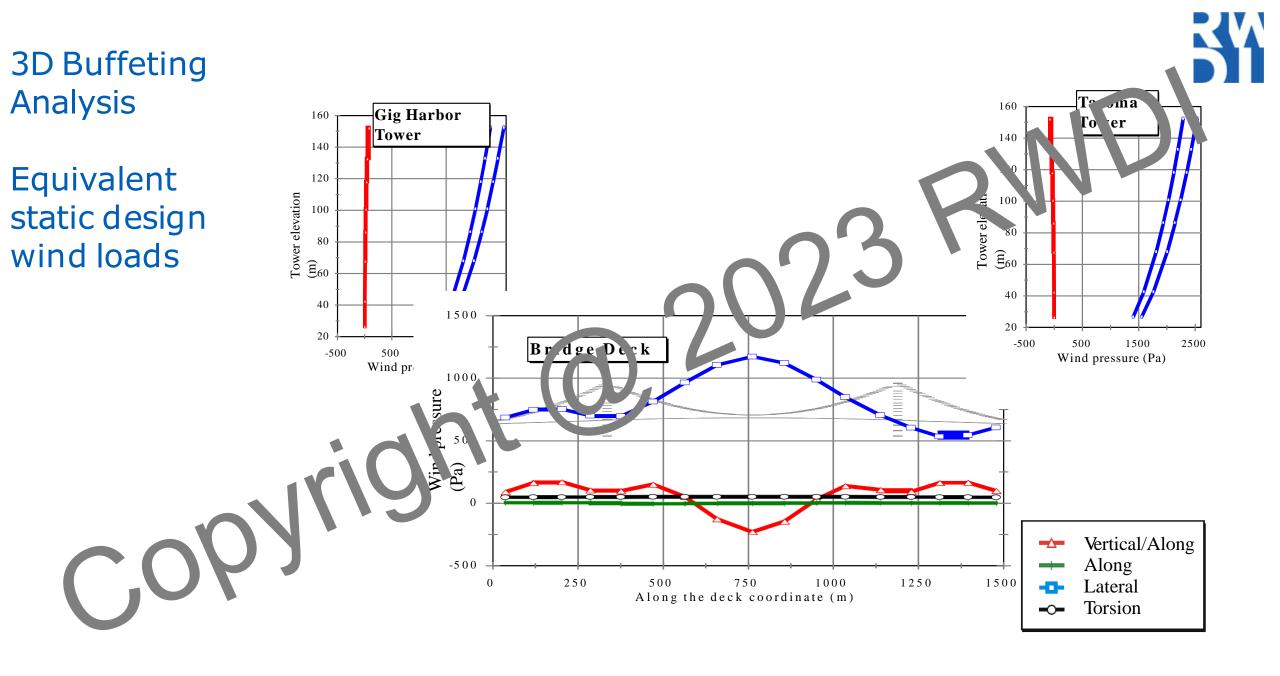
Dynamic information from design team (frequencies, modes, mass distribution)

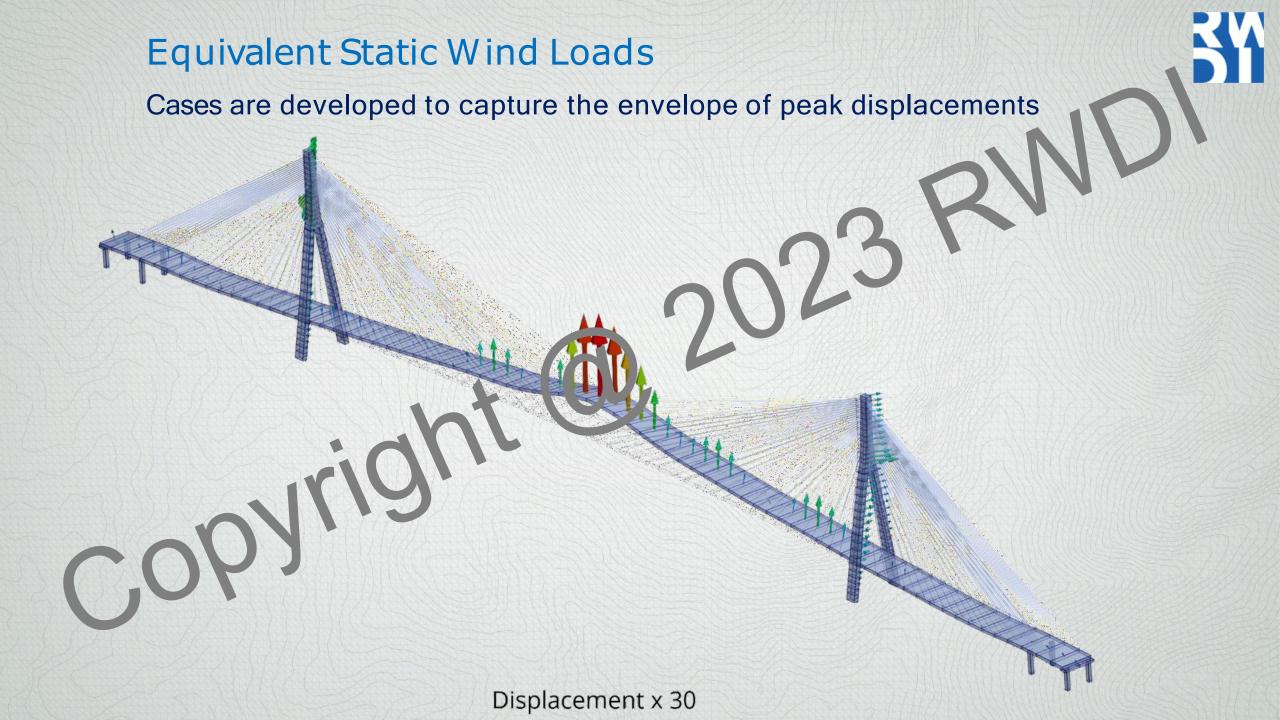
Local wind-climate parameters (wind speed, turbulence, wind profile)

Final cross-section aerodynamic properties (shape, mean forces)

Compute numerically the structural response to fluctuating wind forces









## **Concluding Remarks**

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- Wind effects on bridges are quite different transitional high-rise buildings
- Stability issues are a serious concern at completed and construction stages; wind tunnel lests are required
- Mitigation measures for stability purposes requires wind tunnel testing
- Static force and moment coefficients are also unknown for many cross sections

Minimum studies are to be conducted for design

 Wind climate study, desktop stability assessment, sectional model study, 3D buffeting analysis

